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#### [13-D-02] Numerical Investigation of Disturbance Growth on a Blunt Body in High Enthalpy Hypersonic Flow

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#### Numerical Investigation of Disturbance Growth on a Blunt Body in High Enthalpy Hypersonic Flow

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## Contents

- Boundary Layer Transition (BLT) in re-entry capsules
- Blunt-body paradox
- Direct numerical simulation of disturbance growth
- Measurement of disturbance growth by FLDI



# Thermal protection of re-entry capsules



- Re-entry from Lunar orbit exceeds 11 km/s
- Evaluation of aerodynamic heating is necessary for TPS design

# BLT on front heat shield



- Turbulent heat flux is several times larger than laminar heat flux
- Prediction of BLT and turbulent heat flux is required for TPS design

#### BLT due to modal disturbances

# T-S wave $\rightarrow$ destabilization $\rightarrow$ breakdown $\rightarrow$ turbulence





#### Blunt-body paradox

[1] Reshotko and Tumin, (2000) [2] Farano et al., JFM, (2015)

Why is early transition even though modal disturbance is stable?



- Tollmien–Schlichting (TS) stable
- Görtler stable
- Cross-flow is negligible
- Transient growth<sup>[1]</sup> : Candidate mechanisms of transition
  - > Lift-up effect of streamwise vorticity creates streaks<sup>[2]</sup>
- Transition triggers: wall roughness, freestream disturbances



- Transient growth<sup>[1]</sup> : Candidate mechanisms of transition
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### Effect of roughness on BLT

[3] Hein et al., AIAA, (2018)
[4] Giovanni and Stemmer, JSR, (2018)
[5] Giovanni and Stemmer, JSR, (2019)



#### Isolated roughness

- No growth of mode disturbances
- No transient growth was observed (roughness was too low)



#### **Distributed roughness**

- Hairpin vortex grows
- Chemical non-equilibrium amplifies disturbances Important for high enthalpy flows!

#### Objective

To clarify the transition mechanism and obtain turbulent heat flux in the re-entry capsule, we evaluate the disturbance growth process under high enthalpy conditions using Apollo capsule models with isolated roughness elements

# Numerical method

 $\frac{\partial \boldsymbol{Q}}{\partial t} + \frac{\partial \boldsymbol{F}_i}{\partial \xi_i} + \frac{\partial \boldsymbol{F}_{vi}}{\partial \xi_i} + \boldsymbol{S} = 0 \quad (i = 1, 2, 3) : \text{ 3D general curvilinear coordinate system Navier-Stokes equations}$ 

$$\boldsymbol{Q} = J \begin{bmatrix} \boldsymbol{\rho} \\ \boldsymbol{\rho} \boldsymbol{u}_1 \\ \boldsymbol{\rho} \boldsymbol{u}_2 \\ \boldsymbol{\rho} \boldsymbol{u}_3 \\ \boldsymbol{E} \\ \boldsymbol{Y}_{n-1} \end{bmatrix}, \boldsymbol{F}_i = J \begin{bmatrix} \boldsymbol{\rho} \boldsymbol{U}_i \\ \boldsymbol{\rho} \boldsymbol{u}_1 \boldsymbol{U}_i + \frac{\partial \xi_i}{\partial \boldsymbol{x}_1} \boldsymbol{p} \\ \boldsymbol{\rho} \boldsymbol{u}_2 \boldsymbol{U}_i + \frac{\partial \xi_i}{\partial \boldsymbol{x}_2} \boldsymbol{p} \\ \boldsymbol{\rho} \boldsymbol{u}_3 \boldsymbol{U}_i + \frac{\partial \xi_i}{\partial \boldsymbol{x}_3} \boldsymbol{p} \\ \boldsymbol{\rho} \boldsymbol{u}_3 \boldsymbol{U}_i + \frac{\partial \xi_i}{\partial \boldsymbol{x}_3} \boldsymbol{p} \\ (\boldsymbol{E} + \boldsymbol{p}) \boldsymbol{U}_i \\ \boldsymbol{\rho} \boldsymbol{Y}_{n-1} \boldsymbol{U}_i \end{bmatrix}, \boldsymbol{F}_{i} = -J \frac{\partial \xi_i}{\partial \boldsymbol{x}_j} \begin{bmatrix} \boldsymbol{0} \\ \boldsymbol{\tau}_{j1} \\ \boldsymbol{\tau}_{j2} \\ \boldsymbol{\tau}_{j3} \\ \boldsymbol{\tau}_{jk} \boldsymbol{u}_k + \kappa \frac{\partial T}{\partial \boldsymbol{x}_j} + \sum_s \boldsymbol{\rho} \boldsymbol{v}_{n-1} \boldsymbol{h}_{n-1} \\ \boldsymbol{\rho} \boldsymbol{v}_{n-1} \end{bmatrix}, \ \boldsymbol{S} = -J \begin{bmatrix} \boldsymbol{0} \\ \boldsymbol{0} \\ \boldsymbol{0} \\ \boldsymbol{0} \\ \boldsymbol{s}_{\boldsymbol{Y}_{n-1}} \end{bmatrix}.$$

Inviscid terms	SLAU2 & 7 <sup>th</sup> order Weighted Compact Nonlinear Scheme (WCNS)
Viscous terms	6 <sup>th</sup> order compact difference scheme
Time integration	5-stage 4th-order accuracy Runge-Kutta scheme
Reaction model	Dunn & Kang model (5-species & 17-reaction)

# Computational conditions

Stagnation conditions			Freestream conditions			
$H_{0},\mathrm{MJ/kg}$	$p_0, \mathrm{MPa}$	$T_0, \mathrm{K}$	$u_{\infty}, \mathrm{km/s}$	$p_{\infty}, \mathrm{kPa}$	$T_{\infty}, \mathbf{K}$	$Re_{\infty}$
3.6	17	2968	2.5	1.5	271	2.7E6
6.5	33	4529	3.4	3.5	660	2.4E6
9.2	53	5739	3.9	7.6	1012	2.5E6



Multi-block mesh (total mesh: 70 million)



# Validation: Comparison of bow shock shapes





- Shock wave departure distance is consistent with Schlieren images
- No carbuncles were observed, and robust shock capture was achieved

[6] Ma & Mahesh, JFM, (2022)

#### Forest of hairpin



- Numerous hairpin vortices are formed in the wake of roughness<sup>[6]</sup>
- Hairpin vortex grows once, then starts to decay and disappears

### Enthalpy effect on disturbance growth



- Roughness wake hairpin vortices are reduced under low enthalpy condition
- Density disturbance power is also lower under low enthalpy condition

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#### Density disturbance measurement with FLDI

- Measured density disturbance about 1 mm upstream from model surface with three-channel FLDI
- Not affected by mechanical vibrations of the model and achieves multi-MHz bandwidths







### Power spectrum of density disturbance



- 3MJ: Power tends to decay from midstream to downstream
- 6, 9MJ: Power maintained downstream at the same level as midstream

Tendency to grow more disturbance under higher enthalpy conditions (qualitatively consistent with DNS)

#### Conclusion

To clarify the transition mechanism and obtain turbulent heat flux in the re-entry capsule, we evaluated the disturbance growth process under high enthalpy conditions using Apollo capsule models with isolated roughness elements

- Numerous hairpin vortices were formed in the wake of roughness
- Tendency to grow more disturbance under higher enthalpy conditions
  - > DNS and experimental results were qualitatively consistent
  - > Are high enthalpy conditions more likely to transition?