
Oral presentation | Numerical methods

Numerical methods-VII

Thu. Jul 18, 2024 2:00 PM - 4:00 PM Room A

[11-A-02] An immersed boundary wall-modeled large-eddy simulation approach for low and high-speed flows

*Christoph Brehm¹, Johan Larsson¹, William van Noordt² (1. University of Maryland, 2. University of Oxford)

Keywords: immersed boundary method, turbulent flow, numerical method

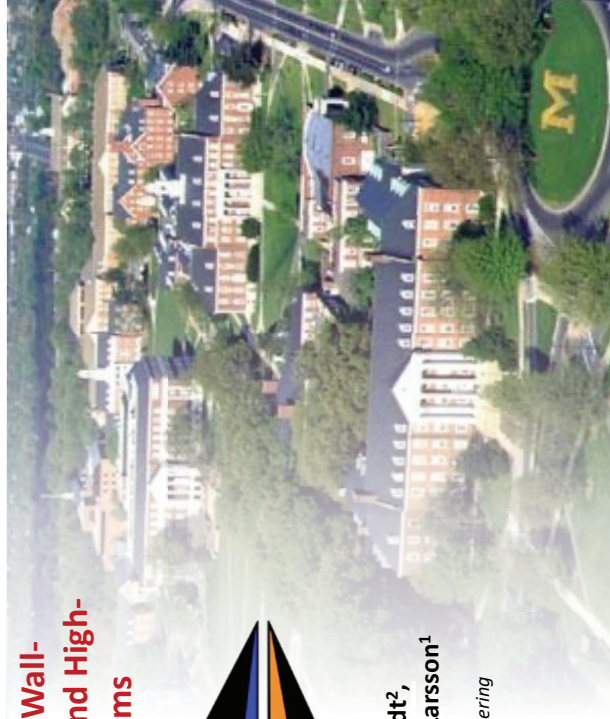
Immersed Boundary Wall-Modeled LES for Low- and High-Speed Flow Problems



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J. McQuaid², S. Ganju¹, & J. Larsson¹

¹Department of Aerospace Engineering
University of Maryland, USA

²Whoosh HPC Lab, LLC, USA



Outline

Brief Overview of Immersed Boundary Methods (IBM)

- Continuous Forcing, Cut-Cell Method, Ghost-Cell Method, & Sharp Finite Difference IBM

Some applications of IBM

- Rocket launch
- Contra-rotating open rotor
- Supersonic parachute inflation
- Wave packet tracking
- Droplet impact

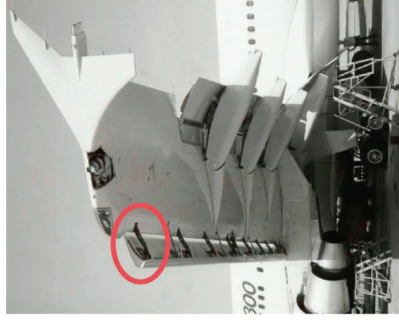
IBM and Wall Modeled LES

- Numerical Implementation
- Some Validation Results + Performance

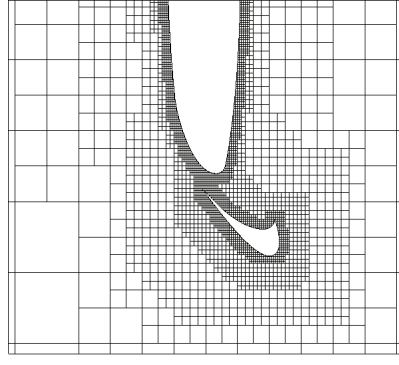
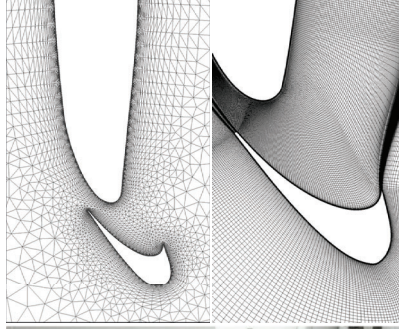
3

Grid Generation

“Real world” hardware.



State-of-the-art meshes around an airfoil with deployed slat.



IBM can facilitate our ability to capture geometrically complex objects.

2

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IBM and Wall Modeled LES

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Historic perspective of our journey to WM-IBM

4



Different IBM Approaches

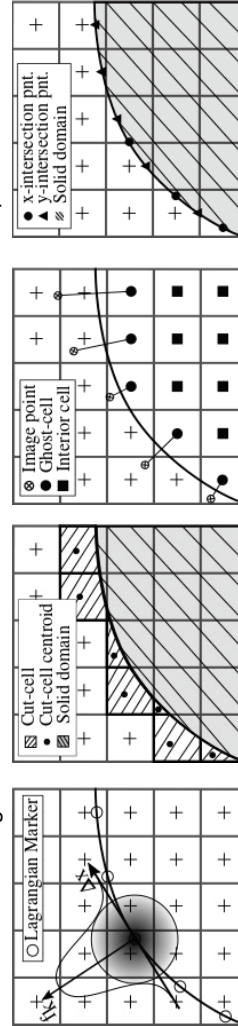
5

ICCFD12



Different IBM Approaches

Continuous Forcing Cut-Cell Method Ghost-Cell Method Sharp Finite Difference IBM



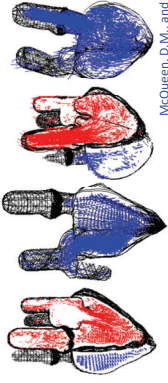
Boustani, Barad, Kiris, & Brehm (2021)

7

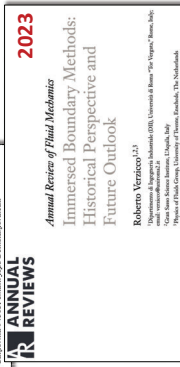
History of IBM

- Introduced in the 70s to simulate the flow in the human heart.
- Heart walls are modelled as elastic membranes.
- The interaction is modelled using a source term added to the governing equations. Peskin (1972,1977)
- IBMs appeared in many different forms:
 - Direct Forcing (Mohd-Yusof (1997), Goldstein et al. (1993))
 - Ghost-Cell Method (Fedkiw et al. (1999), Majumbar et al. (2001), Ferziger & Peric(1996), Iaccarino & Verzicco (2003), Mittal(2004)
 - Immersed Interface Method (Lee & Leveque (2003), Linnick & Fasel (2005))
 - Distributed Lagrange Multiplier (Glowinski et al. (1998), Projection Approach Taira & Colonius (2007))
 - Cut Stencil Method (Green et al. (2016), Duan et al. (2012))
 - Embedded Boundary Method (Balaram (2003), Yang & Balaram (2005), Colletta et al. (2006), Schwartz et al. (2006), Barad et al. (2005))
 - Cut-Cell/Fluid Method (Clarke et al. (1986), Udaykumar et al. (2001,2001), Ye et al. (1999), Berger & Atoms (1998), Berger (1990), Meinke et al. (2013), Meyer et al. (2010), Melton et al. (1995), Orley et al. (2015), Pogorelov et al. (2015))
 - SBP+SATS (Mattson & Almqvist (2016))
 - Discontinuous Galerkin (Müller et al. (2016))
 - etc.

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McQueen, D.M., and Peskin, C.S. (1995)



6



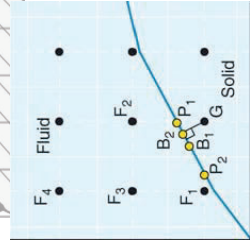
Different IBM Approaches

Continuous Forcing Cut-Cell Method Ghost-Cell Method Sharp Finite Difference IBM

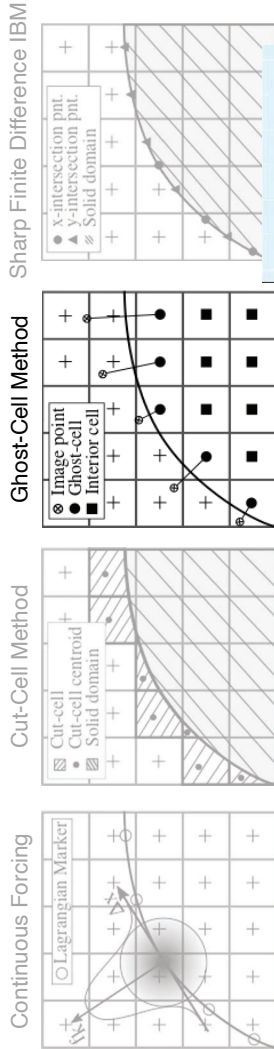


- Is the most popular IB approach because it is very simple to implement
- Many papers have been published on ghost-cell methods (Majumdar et al. (2001), Iaccarino & Verzicco (2003), Iaccarino et al. (2003), Mittal et al. (2004), Kalitzin et al. (2003), ...)
- Boundary condition on the IB is enforced through the use of "ghost cells"
- Interpolation scheme that implicitly incorporates the boundary condition on the IB is devised

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Different IBM Approaches



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ICCFD12

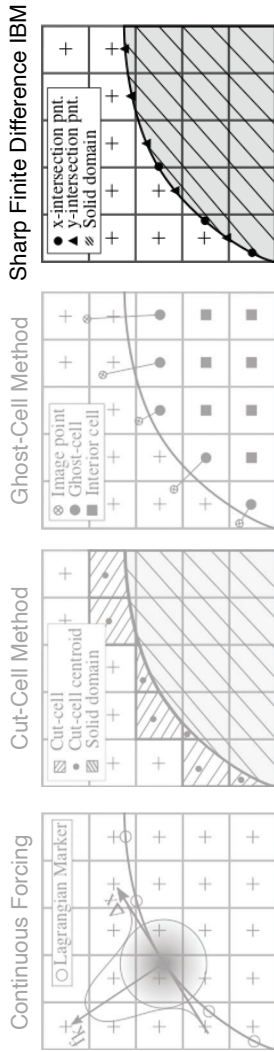
Different IBM Approaches



- Direct enforcement of boundary conditions at the wall
- Many different flavors have been developed
- Jump corrected FD schemes (Wiegmann & Bube (2000), Linnick & Fasel (2004), ...)
- Use of irregular finite difference operators (Brehm & Fasel (2013, 2015), Duan et al. (2010), ...)

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Different IBM Approaches



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Early Applications of IBM

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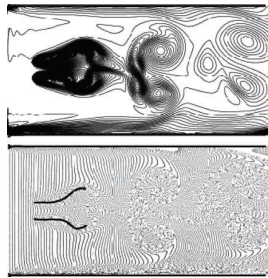
IBM Solutions Highlighted in Annual Review 2005



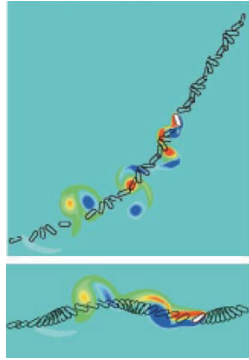
Khalighi et al., 2001
Verzicco et al., 2002

Non-uniform Cartesian mesh

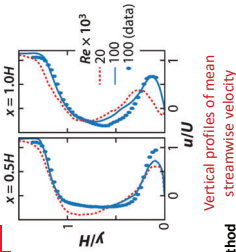
Streamtraces of mean flow at $Re = 20$
Flow around a 3D model road vehicle using the immersed boundary method



Clapping motions of two filaments in a flowing soap film Zhu, 2003



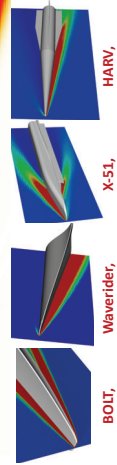
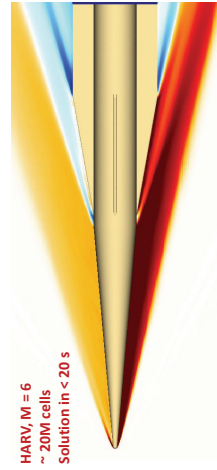
Simulation of a plate in free fall (cut-cell method) Mittal et al., 2004



Vertical profiles of mean streamwise velocity

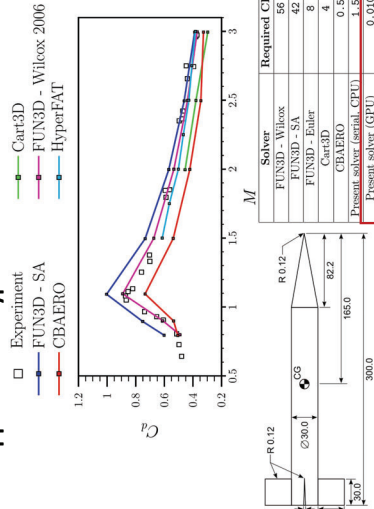
Hypersonic Vehicle Performance Analysis and Trajectory Simulations

Small Business Innovation Research Phase I/II Project:
Digital Engineering - A Fully-Automated Simulation Approach for Hypersonic Vehicles



Solutions for typical hypersonic vehicles can be obtained in < 1min (additional optimization possible)!

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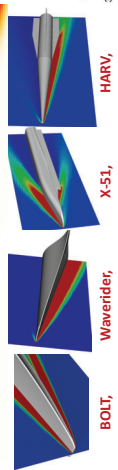
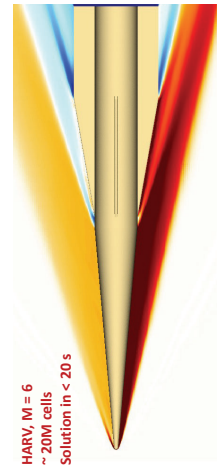


- Performance comparison for ANF geometry:
- GPU + FWSI dramatically outperforms other codes

Solver	Required CPU-hours
FUN3D - Wilcox	56
FUN3D - SA	42
FUN3D - Euler	8
Cart3D	4
CBAERO	0.5
Present solver (serial, CPU)	1.5
Present solver (GPU)	0.0108

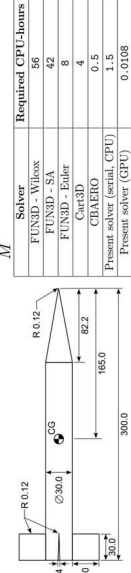
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What was next?

Can we obtain truly higher-order IBMs?

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Basic Idea of Stability Enhancement

- Initial observation:
"Stability of numerical scheme can be formulated as N-dimensional optimization problem"
(N=number of irregular grid points)

- Derivation of stencil coefficients:

- Enforce order-of-accuracy

$$\tau_1 = \left(-c_x \frac{\partial \phi}{\partial x} + \frac{\partial}{\partial x} \left(\beta \frac{\partial \phi}{\partial x} \right) + f \right)_{x=x_i} - \left(\hat{\phi}_B \tilde{\alpha}_1 + \hat{\phi}_1 \tilde{\alpha}_2 + \hat{\phi}_{i+1} \tilde{\alpha}_3 + \hat{\phi}_{i+2} \tilde{\alpha}_4 + \hat{\phi}_{i+3} \tilde{\alpha}_5 + C \right)$$

- Additional grid point is needed to introduce free parameter
- Objective function depends on the nature of the PDE, e.g., $\lambda_{r,\max}$ or $\rho(A)$

$$\frac{\partial \phi}{\partial t} = -c_x \frac{\partial \phi}{\partial x} + \frac{\partial}{\partial x} \left(\beta \frac{\partial \phi}{\partial x} \right) + f \xrightarrow{\text{discr.}} \underline{\mathbf{B}} \hat{\phi}^{n+1} = \underline{\mathbf{A}} \hat{\phi}^n + \hat{\mathbf{f}}$$

- Extract perturbation of irregular finite difference stencil (assume $\underline{\mathbf{B}}=\mathbf{I}$)

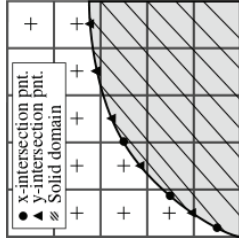
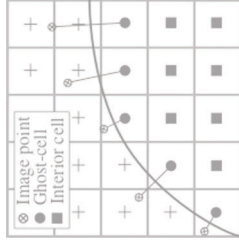
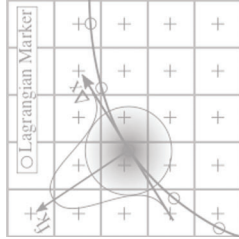
$$\underline{\mathbf{A}} = \underline{\mathbf{E}} \underline{\mathbf{A}}_{id} \xrightarrow{\text{cond.}} \rho(\underline{\mathbf{E}}) \leq 1$$

Brehm & Fasel (ICP 2013, 2015), applications: Brehm, Barad, & Kirs (ICP 2018, JFH 2017), Brehm, Barad, Housman & Kirs (JFM 2016)

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Different IBM Approaches

Continuous Forcing Cut-Cell Method Ghost-Cell Method Sharp Finite Difference IBM



- Direct enforcement of boundary conditions at the wall

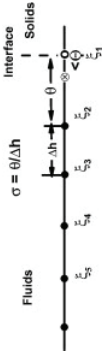
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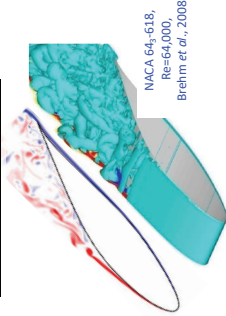
Brehm & Fasel (2013,2015), Duan et al. (2010), ...





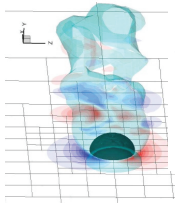
Simple IBM Problems – Low Speed

Q-criterion & streamwise vorticity



NACA 64-618, Re=64,000, Brehm et al., 2008

Q-criterion & streamwise velocity

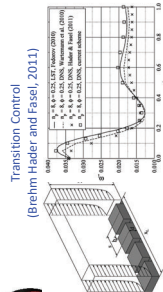


unsteady sphere flow, Re=1,000 (Brehm and Fasel, 2011a, 2011b)

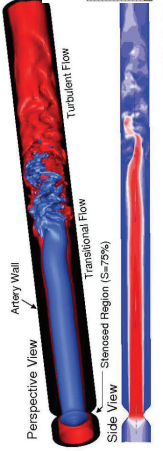
Q-criterion (Q=1)



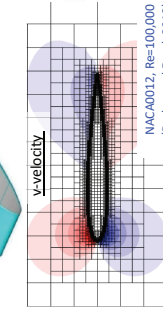
NACA0015, Re=1,000-10,000 (Brehm and Fasel, 2011a, 2011b)



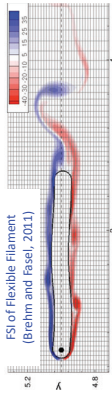
Aortic Dissection Simulation (Brehm Hader and Fasel, 2011)



persistile stenotic flow, Re=500, S=75%, V/R=8, Brehm et al. (2011, 2012)



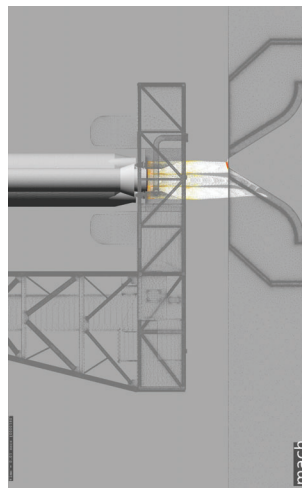
FSI of flexible filament (Brehm and Fasel, 2011)



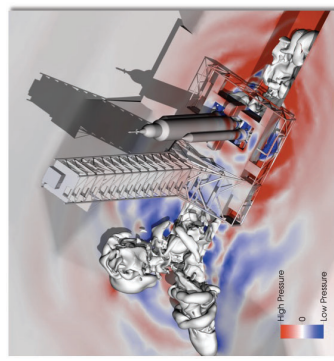
flow past distributed roughness, Brehm et al. (2011), 0.27 experiments by Prof. Gaster, London, UK

Can IBMs be used for practically relevant aerospace problems?

Rocket Launch Simulations



Technical reports: NASA-TM October 15 2014 ARC-E-DAA-TN7327 and ARC-E-DAA-TN10931



Kiris et al. (2015)

- Utilization of Immersed boundary method for design of launch infrastructure at NASA KSC
- Ignition over-pressure (IOP) analysis
- Multi-physics simulation (multi-species, multi-phase, etc.)
- Automatic volume grid generation from surface triangulation
- Adaptive mesh refinement (AMR) for tracking flow features with local refinement (gradient, entropy adjoint, and geometry based)

Contra-Rotating Open Rotor

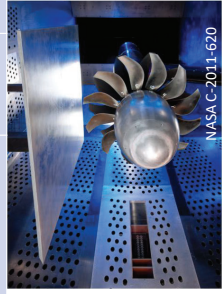
Low Speed (Take-Off)
(9 x 15 Low-Speed Wind Tunnel)



High Speed (Cruise)
(8 x 6 Supersonic Wind Tunnel)



Cases	Low Speed	High Speed
Rotation Speed [RPM]	6303/6303	6848/6848
Blade Setting (fwd/aft) [°]	40.1/40.8	64.4/61.8
Mach	0.20	0.78

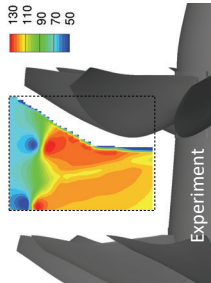


Brehm et al. (ICP 2019)

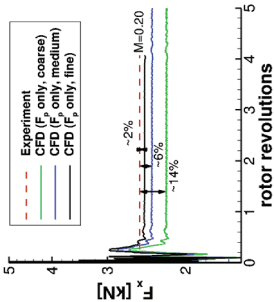


Contra-Rotating Open Rotor

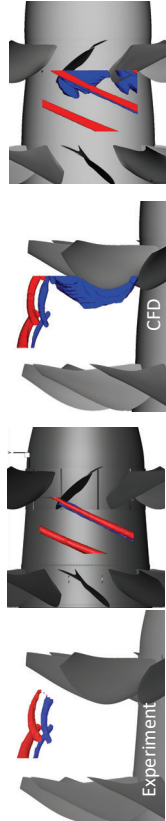
Velocity Magnitude Contours



Trust Comparison



Iso-surface of velocity magnitude with $|v|/V_\infty=0.84$ (red) and 1.91 (blue)



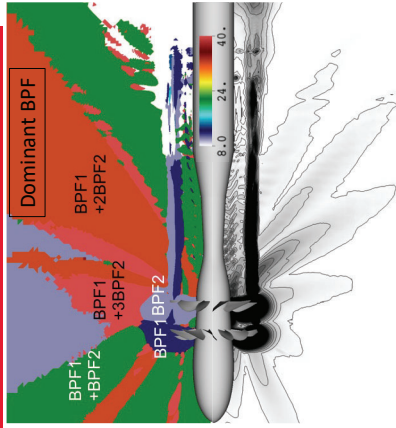
Brehm et al. (JCP 2019)

Courtesy of NASA Ames Research Center!

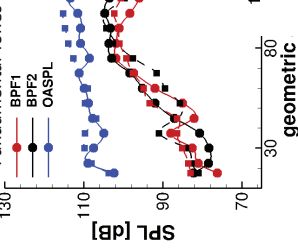
25



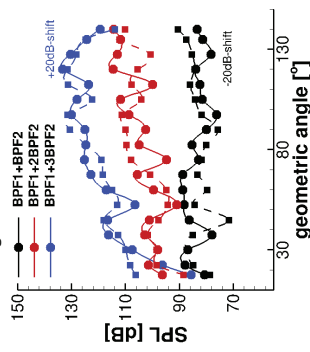
Contra-Rotating Open Rotor



Fundamental Tones



Higher-Order Interactions



Normalized Max. Pressure Amplitude

Brehm et al. (JCP 2019)

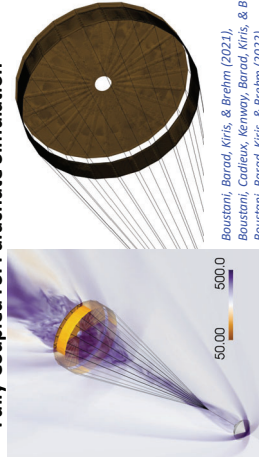
Courtesy of NASA Ames Research Center!

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Supersonic Parachute Inflation

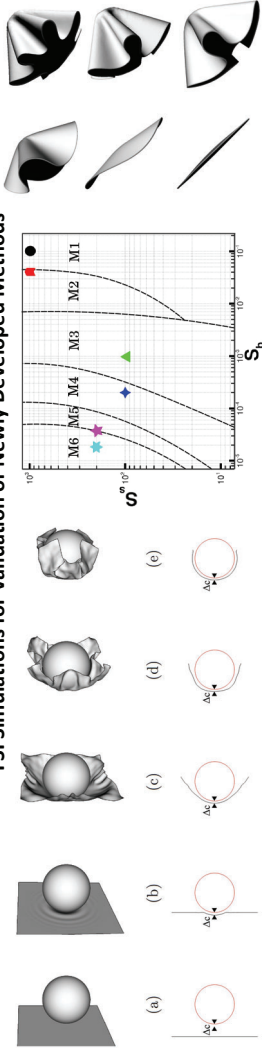
Fully-Coupled FSI Parachute Simulation



Boustani, Barad, Kirs, & Brehm (2021)
Boustani, Cadieux, Kenway, Barad, Kirs, & Brehm (2022),
Boustani, Barad, Kirs, & Brehm (2022)

ASPIRE Parachute Test

FSI Simulations for Validation of Newly Developed Methods



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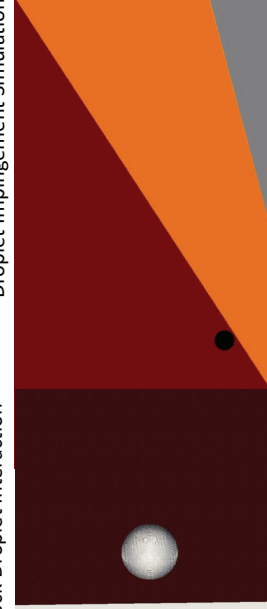


Droplet Impingement

Droplet Impingement on SRB

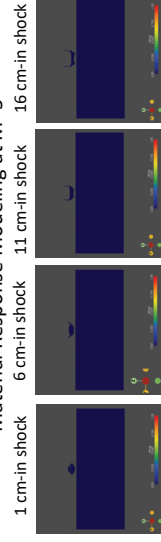


3D Shock-Droplet Interaction



Droplet Impingement Simulation

Material Response Modeling at M=5



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Application of IBM to RANS

... skipping this in the interest of time

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Finally! Application of IBM in context of WMLES

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History of IBM

Annu. Rev. Fluid Mech. 2005. 37:239-61
doi: 10.1146/annurev.fluid.37.061903.175743
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2005

IMMERSED BOUNDARY METHODS

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2023

Annual Review of Fluid Mechanics

Immersed Boundary Methods: Historical Perspective and Future Outlook

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¹Dipartimento di Ingegneria Industriale (DII), Università di Roma "Tor Vergata", Rome, Italy;
email: verzicco@uniroma2.it

²Gran Sasso Science Institute, L'Aquila, Italy

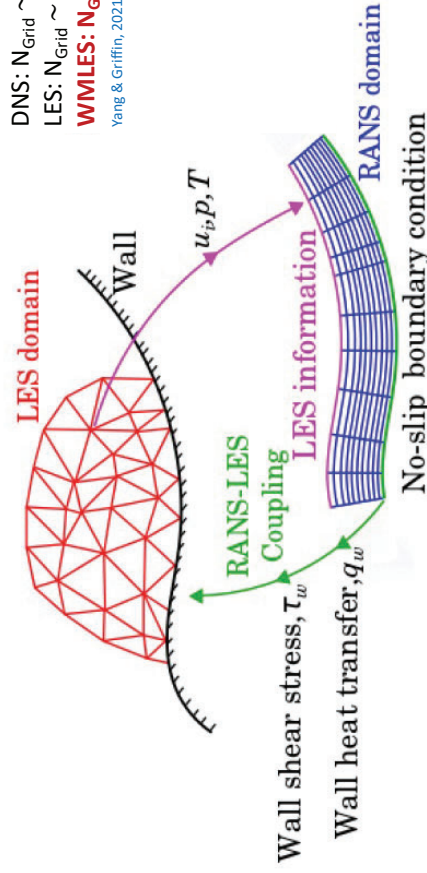
³Physics of Fluids Group, University of Twente, Enschede, The Netherlands

[...] **High-Reynolds number flows constitute one of the main limitations** of IBMs owing to the resolution of thin wall shear layers, which cannot benefit from anisotropic grid refinement at the boundaries. To alleviate this weakness, researchers have developed [...]



Wall Model Coupling to LES Domain

DNS: $N_{Grid} \sim Re_L^{2.91}$
LES: $N_{Grid} \sim Re_L^{2.72}$
WMLES: $N_{Grid} \sim Re_L^{1.14}$
Yang & Griffin, 2021

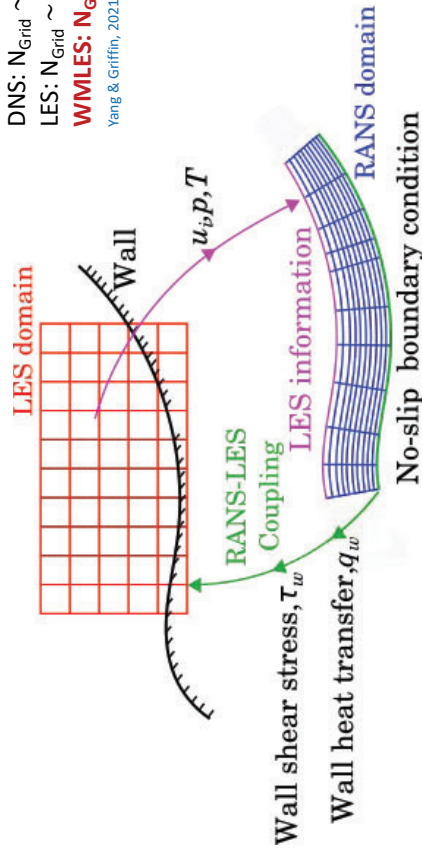


Adjusted from Bodart & Larsson (2011)

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DNS: $N_{Grid} \sim Re_L^{2.91}$
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 Yang & Griffin, 2021



Adjusted from Bodart & Larsson (2011)

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The main objectives of this work are to assess:

1. the effect of **boundary closures** used for IBMs when coupled with wall model
2. the effects of **non grid aligned boundaries**

$$+ (i,j) \\ + (i,j-1)$$

35

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$$+ (i,j) \\ + (i,j-1) \\ M_x = \frac{\partial(\rho uv)}{\partial y} \\ M_y = \frac{\partial(\rho u^2 + p)}{\partial y}$$

36



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$$\begin{array}{c}
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 \hline
 + \text{ (i,j-1)}
 \end{array}
 \quad
 \begin{array}{l}
 M_x = \frac{\partial(\rho uv)}{\partial y} \\
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 \end{array}$$

37

ICCFD12



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$$\begin{array}{c}
 + \text{ (i,j)} \\
 \hline
 + \text{ (i,j-1)}
 \end{array}
 \quad
 \begin{array}{l}
 M_x = \frac{\partial(\rho uv)}{\partial y} = \frac{(\rho uv)_{i,j+1/2} - (\rho uv)_{i,j-1/2}}{\Delta y} \rightarrow 0 \\
 M_y = \frac{\partial(\rho v^2 + p)}{\partial y}
 \end{array}$$

$$v_{i,j} = -v_{i,j-1} \rightarrow v_{i,j-1/2} = \frac{v_{i,j} + v_{i,j-1}}{2} = 0$$

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2. the effects of **non grid aligned boundaries**

$$\begin{array}{c}
 + \text{ (i,j)} \\
 \hline
 + \text{ (i,j-1)}
 \end{array}
 \quad
 \begin{array}{l}
 M_x = \frac{\partial(\rho uv)}{\partial y} \\
 M_y = \frac{\partial(\rho v^2 + p)}{\partial y}
 \end{array}$$

$$v_{i,j} = -v_{i,j-1} \rightarrow v_{i,j-1/2} = \frac{v_{i,j} + v_{i,j-1}}{2} = 0$$

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Objectives

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1. the effect of **boundary closures** used for IBMs when coupled with wall model
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 + \text{ (i,j)} \\
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 \quad
 \begin{array}{l}
 M_x = \frac{\partial(\rho uv)}{\partial y} = \frac{(\rho uv)_{i,j+1/2} - (\rho uv)_{i,j-1/2}}{\Delta y} \rightarrow 0(\Delta x^2) \neq 0 \\
 M_y = \frac{\partial(\rho v^2 + p)}{\partial y}
 \end{array}$$

$$v_{i,j} = -v_{i,j-1} \rightarrow v_{i,j-1/2} = \frac{v_{i,j} + v_{i,j-1}}{2} \neq 0$$

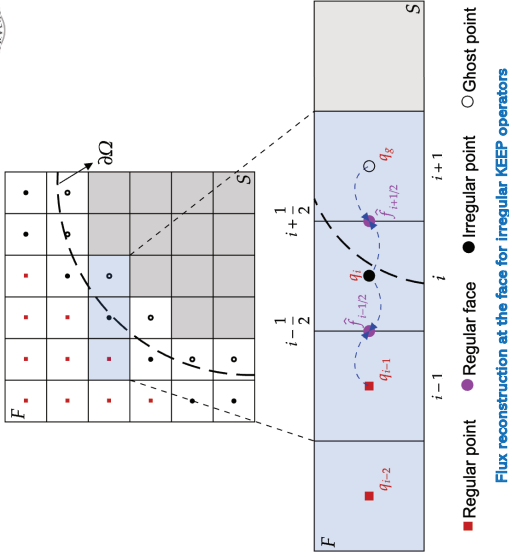
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Numerics – Irregular Convective Terms

- Like regular treatment with order-reduction at IB
 - 4th order kinetic energy and entropy preserving (KEEP) scheme^{18,19}
 - stability and reduction of spurious noise
 - third-order upwinding for dissipation

$$\hat{f}(c) = (1 - \alpha)\hat{f}_{KEEP} + \alpha \hat{f}_{aiss}$$

- Dissipation added using specially designed upwind operators³
 - One ghost used
 - Flux-vector splitting
 - Upwind biased
- Specialized procedures for ghost-cell filling



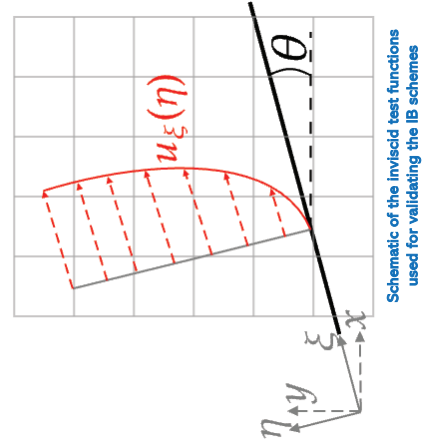
³van Noordt, W., Ganju, S., & Brehm, C., JCP, 2022

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Numerics – Inviscid Tests

- Immersed boundaries can cause large errors for non-aligned Cartesian grids
 - Series of test functions used to assess the effect of IB operators on the solution
 - Flat plate geometry
 - Several angles of IB inclination (θ) tested
 - Simulations use 2nd-order KEEP flux with no dissipation
- Test functions
 - Linear: $\bar{u}_t = a\eta + b$
 - Quadratic: $\bar{u}_t = a\eta^2 + b\eta + c$
 - Laminar profile (Blasius)
 - Turbulent profile (Reichardt)
- Test functions rotated into a local coordinate system (ξ, η) based on the local IB geometry
- Simulations are run until flow has settled

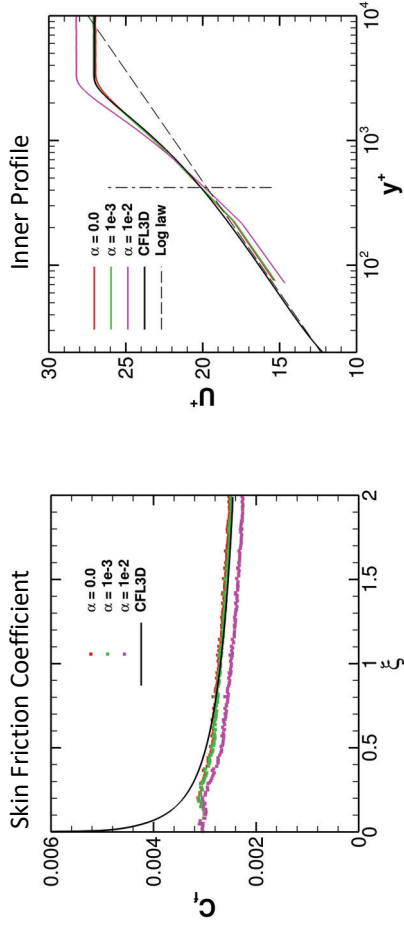


Ganju, van Noordt, & Brehm (submitted to JCP)

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Effects of Dissipation

Flat plate turbulent boundary layer flow (IBM-WM-RANS)



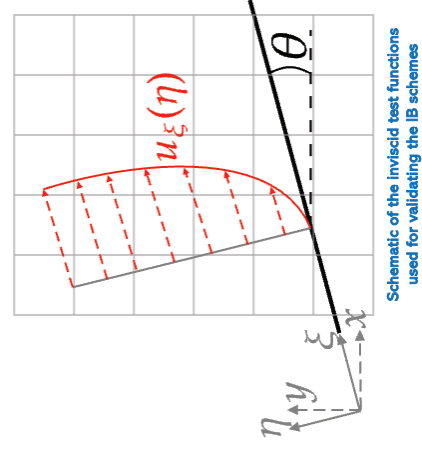
Ganju, van Noordt, & Brehm (submitted to JCP)

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<https://turbmodels.larc.nasa.gov/flatplate.html>

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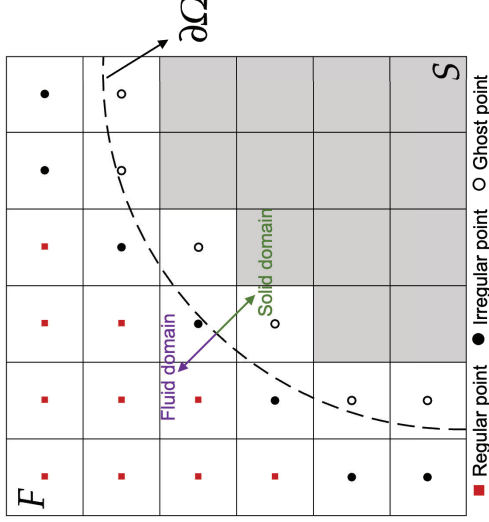
Inviscid Tests – Reichardt Profile

Reichardt profile

- Mimics a turbulent profile
- Freestream adjusted to better approximate boundary layer profile
- Very strong gradients near the wall

$$\vec{u}_{t,g} = c_1 \vec{u}_{t,1} + c_2 \vec{u}_{t,2}$$

- Extrapolate 1: $c_1 = 0, c_2 = 1$
- Extrapolate 2: $c_1 = \frac{d_1}{d_1 - d_2}, c_2 = 1 - \frac{d_g}{d_1 - d_2}$



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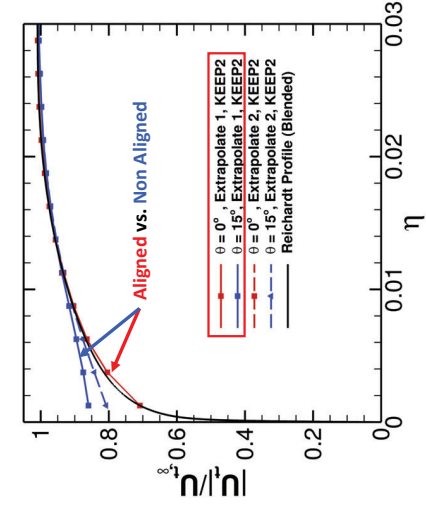
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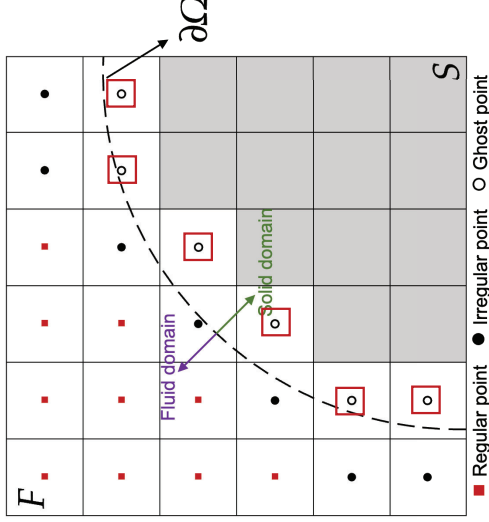
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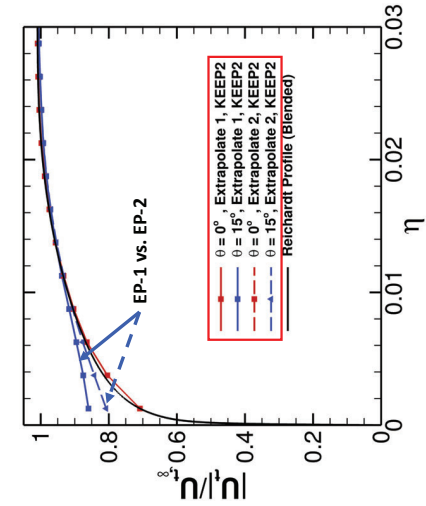
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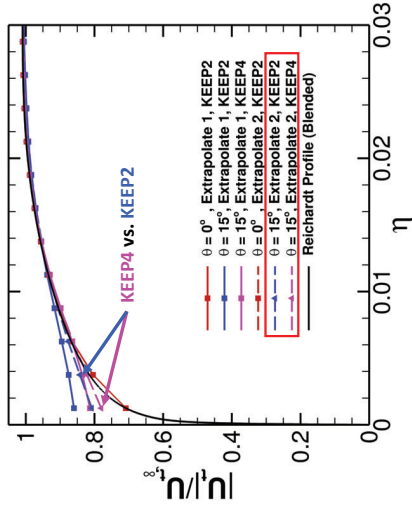
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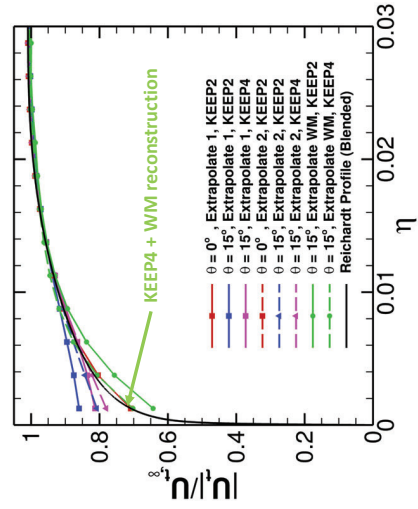


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- Extrapolate WM
 - $\vec{u}_t = \vec{u}_{t,1} - m_{WM}(d_1 + d_g)$
 - Cartesian grid is severely under-resolved
 - Wall-model gradient is a better approximation of the **mean profile**

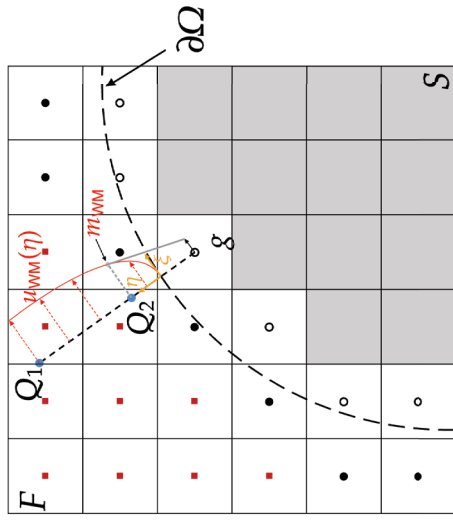


Ganjju, van Noordt, & Brehm (submitted to JCP)

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Inviscid Tests – Reichardt Profile

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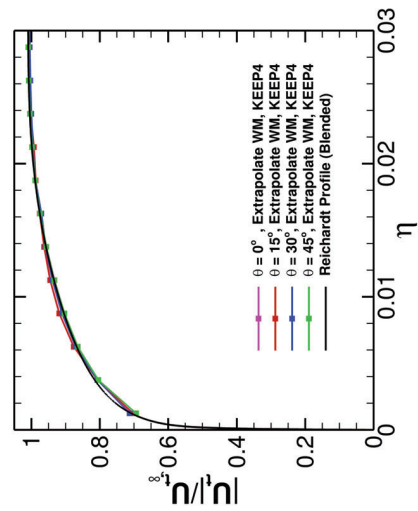


Ganjju, van Noordt, & Brehm (submitted to JCP)

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Inviscid Tests – Reichardt Profile

- Reichardt profile
 - Mimics a turbulent profile
 - Freestream adjusted to better approximate boundary layer profile
 - Very strong gradients near the wall
- Varying domain inclination
 - Different angles of inclination tested
 - Coarse grid used
 - 4th-order KEEP scheme (regular)
 - Extrapolate WM BC

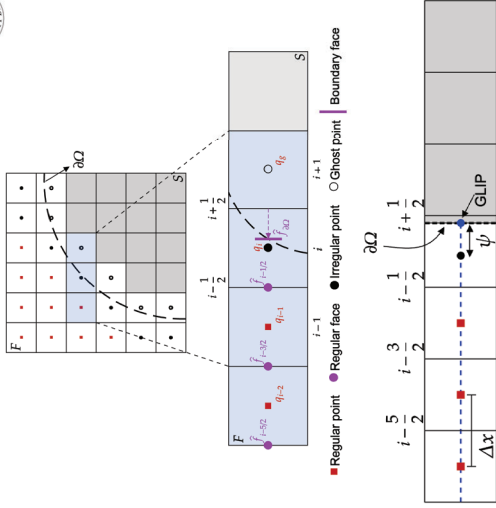


Ganjju, van Noordt, & Brehm (submitted to JCP)

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Numerics – Irregular Viscous Terms

- Viscous fluxes are specified at grid-line intersection points
 - Intersection of the line formed by the cell-centers and the IB
 - $\hat{f}_{\Omega}$ is obtained from the wall-model
 - Ghost-point is not used for evaluation of viscous fluxes
- Flux divergence at grid point i is evaluated as follows
 - Intersection of the line formed by the cell-centers and the IB
 - $\frac{\partial \hat{f}}{\partial x_i} = a\hat{f}_{\Omega} + b\hat{f}_{i-1/2} + c\hat{f}_{i-3/2} + d\hat{f}_{i-5/2}$
 - 2nd-order flux divergence
 - Trying to mimic telescoping sum property



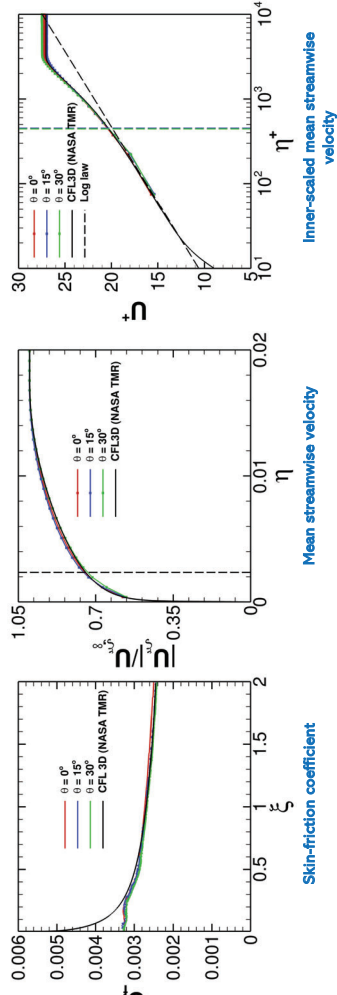
³van Noordt, W., Ganju, S., & Brehm, C., JCP, 2022

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Results – WMRANS of Turbulent Boundary Layer

- Re-visit the WMRANS turbulent layer case from NASA-TMR website
 - Numerical experiments show similar errors when using 2nd order KEEP operator in the regular cells
 - Extrapolate WM BC performs better than other BCs



Ganju, van Noordt, & Brehm (submitted to JCP)

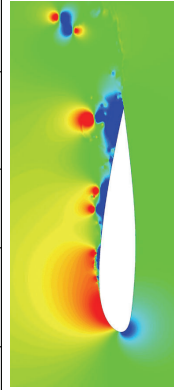
<https://turbomodels.larc.nasa.gov/flatplate.html>

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Results – A-Airfoil

- Turbulent flow past A-Airfoil (recent AIAA paper)
- Flow features:
 - Non-alignment of grid and IB
 - Non-equilibrium flow effects – strong pressure gradients
- Part of the High-Fidelity CFD Verification Workshop⁴

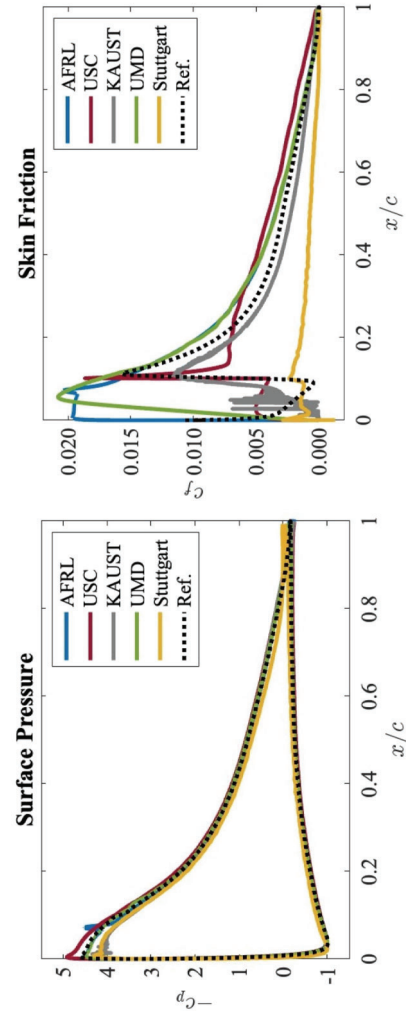
P_{∞} (Pa)	T_{∞} (K)	M_{∞}	Re_1 (m^{-1})	α
101327.0	300.0	0.15	10^7	13.3°



⁴Tamaki & Kawai, AIAA, 2023

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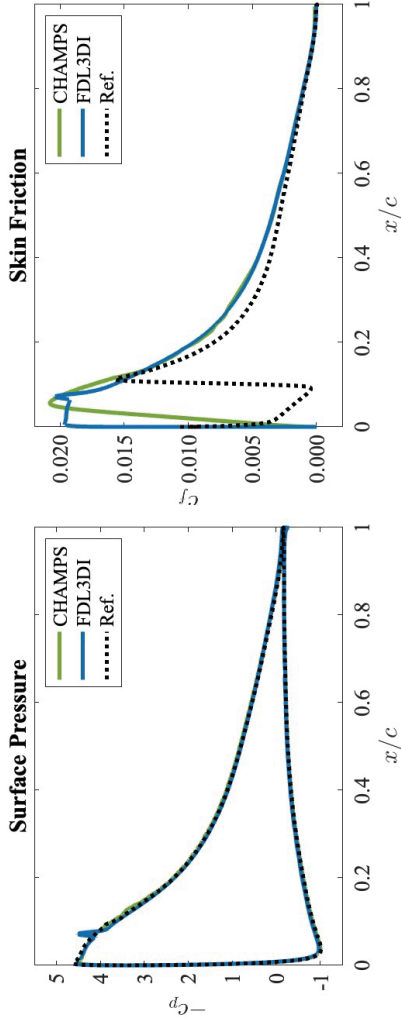
WM Workshop Results – A-Airfoil



Garmann, Larsson, Brehm, et al. "Summary of the Wall-Modeled LES Test Suite from the 2024 AIAA High-Fidelity CFD Verification Workshop," AIAA Aviation 2024

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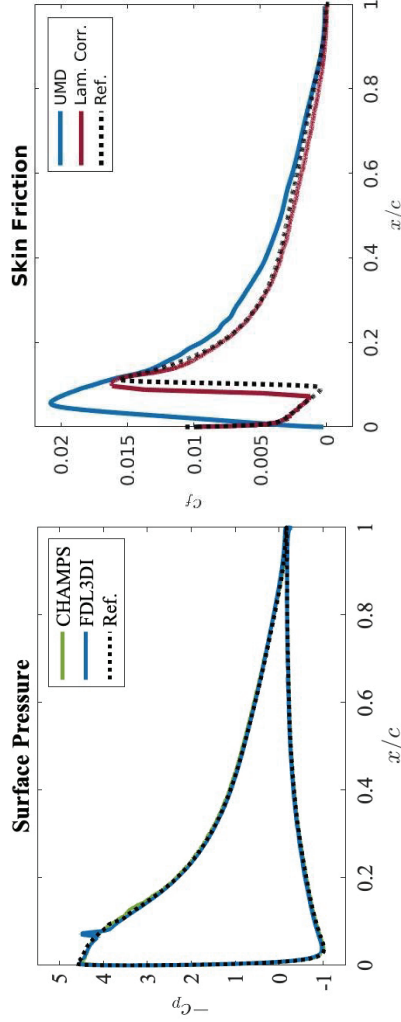
Results – A-Airfoil



Thanks to Dr. Dan Garmann and Dr. Matthew Schwartz for sharing FDL3DI results!!!

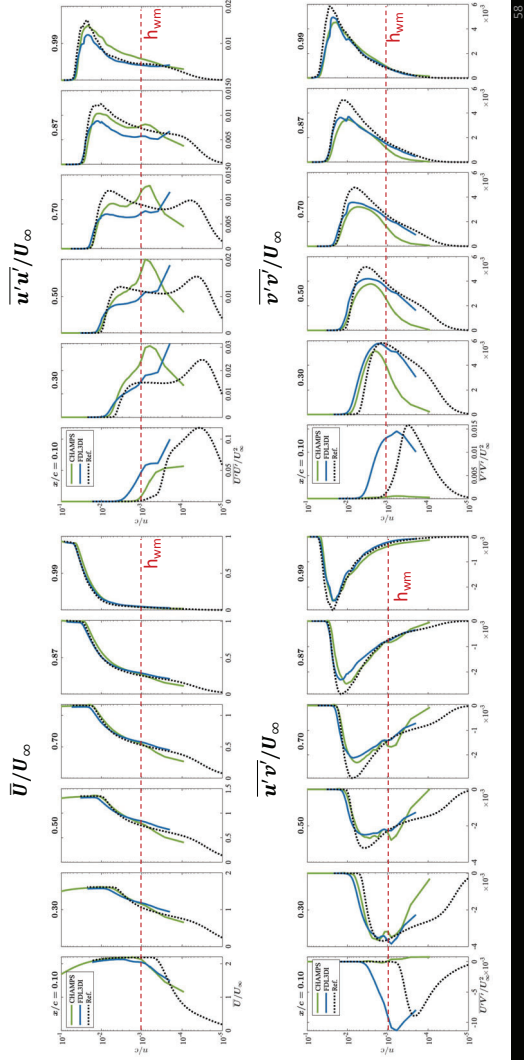
Garmann, Larsson, Brehm, et al. "Summary of the Wall-Modeled LES Test Suite from the 2024 AIAA High-Fidelity CFD Verification Workshop." AIAA Aviation 2024

Laminar BL treatment – A-Airfoil



Hussain, Ganju, Batstone, van Noordt, Larsson & Brehm, "Wall-modeled large eddy simulation of the A-airfoil using body-fitted and immersed-boundary codes," AIAA Aviation 2024

Results – A-Airfoil



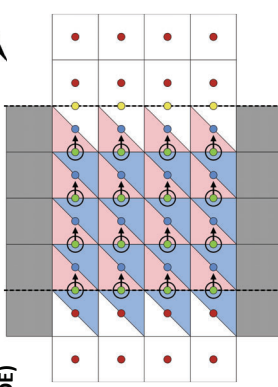
A Note on GPU Performance

Full re-write of CHAMPS within C++20 using generic GPU backend (SPADE)

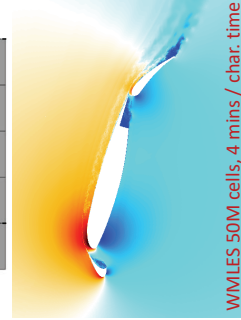
- Low-memory implementation allows for efficient GPU memory usage:
 - approx 8-16M cells / GB of GPU memory
- All schemes, source terms, and boundary conditions written generically with no performance loss
- Compute bound GPU kernels, including for single-precision calculation
- Mixed-precision approach for handling geometry queries and sampling
- Anisotropic mesh refinement to allow high aspect ratio cells / domains

Potential for enabling rapid, high-fidelity analysis:

- 2x RTX 4090, 48GB = 400-500 million cells on a single workstation
- Depending on case complexity, 1.8-2.7 billion cells updated per second with 3-stage explicit scheme
- Approx. 140x faster than previous CPU implementation



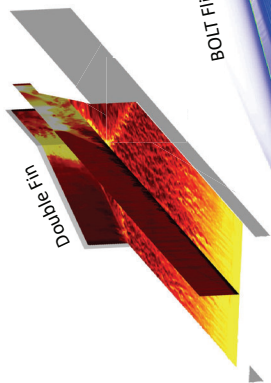
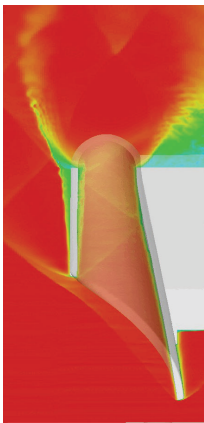
Flux divergence algorithm utilizing optimal memory layout on GPUs



WMLES 50M cells, 4 mins / char. time

High-Speed Applications

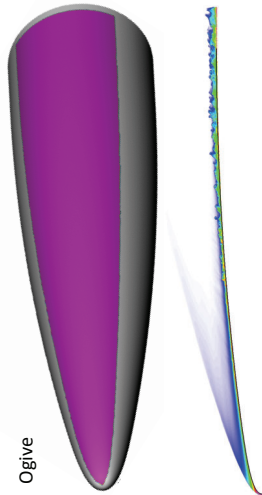
Scramjet inlet



BOIT Flight Vehicle



Ogive



Ramjet

